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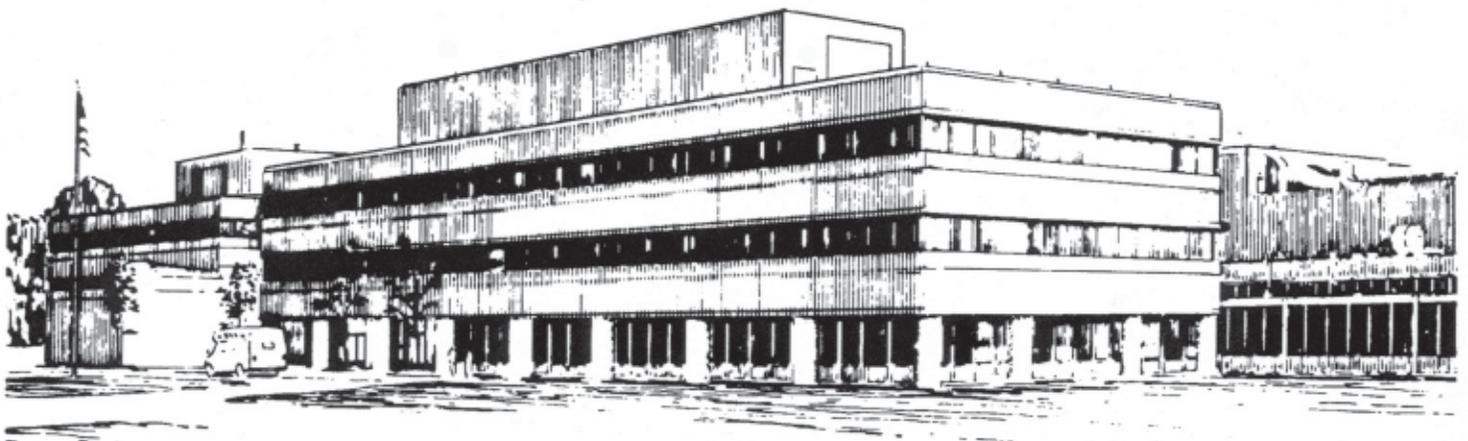
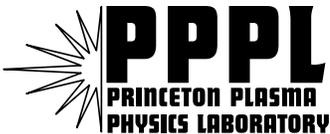
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**Simulations of Temperatures in Burning Tokamak Plasmas
Using the GLF23 Model in the TRANSP Code**

by
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Simulations of temperatures in burning Tokamak plasmas using the GLF23 model in the TRANSP code

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The GLF23 prediction model, incorporated in the TRANSP plasma analysis code, is used to predict temperatures for burning plasmas in the proposed FIRE and ITER-FEAT Tokamaks. Flat electron density profiles with various central values are assumed. Scaling of the fusion power P_{dt} and gain Q_{dt} with density and pedestal temperature are given. Helium ash transport and sawtooth effect P_{dt} in long duration ITER-FEAT plasmas. Classification: MO (Reactor Physics and Design)

1. Introduction

Nest-step tokamaks for burning plasma experiments are being proposed. In order for these experiments to provide clear results for alpha heating studies and for reliable extrapolations to fusion power reactors, the dt fusion power P_{dt} and fusion gain $Q_{dt} = P_{dt} / P_{aux}$ should be large. Two of the proposed next-step tokamaks, FIRE [1] and ITER-FEAT [2] have the goal of achieving $Q_{dt} = 10$. The plasma durations are projected to about 20 and 400 s, respectively.

There are many uncertainties in extrapolating present tokamak experiments to those envisioned in burning Tokamak plasmas. One of the theory-based predictive models, GLF23 [3], is promising since it has been successful in simulating T_e and T_i in present plasmas. This model has been incorporated into the TRANSP plasma analysis code [4], which has strong capabilities for simulating the heat depositions in present experiments.

The goal of this paper is apply the TRANSP-GLF23 code to simulate T_e , T_i , P_{dt} , and Q_{dt} in FIRE and ITER-FEAT plasmas. Peaked electron density profiles have been proposed for FIRE since they are often associated with high energy confinement in present experiments, but there is uncertainty as to whether they can be created in the high density and temperature plasmas required for high Q_{dt} . To be conservative about the technological difficulties in generating peaked density profiles, very broad n_e profiles, similar to those envisioned for the ITER-FEAT tokamak [2], are assumed.

Other studies have used the GLF23 model to predict temperatures in FIRE and ITER-FEAT plasmas, using, for instance, the TSC [5] code. The TRANSP code uses a number of difference techniques, such as Monte Carlo techniques [6] to calculate the fusion alpha heating, and the SPRUCE full-wave, reduced order code [7] to calculate the ICRH heating. Also the accumulation of the alpha ash is computed. The results of this study for FIRE are optimistic than in that the height of the pedestal temperature needed for $Q_{dt} \geq 10$ is relatively low, around 2.5 keV. The

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results for ITER-FEAT indicate that the time scale for P_{dt} to increase can be very long due to the slow accumulation of the alpha ash.

2. FIRE Plasmas.

FIRE [1] is designed to have normal-conducting magnets, and a double-null divertor geometry. The normal heating scheme is ICRH at a frequency of 100 MHz to resonate with small concentrations of He^3 and large concentrations of T on axis. The heating power P_{RF} is assumed to start high (20 MW) early in the discharge to provoke the L to H-mode transition, and then is lowered to 11.5 MW as the alpha heating increases, to maintain the H-mode. The assumed evolution of the heating powers are shown in Fig. 1. The ICRH heating and alpha parameters for a similar FIRE H-mode plasma are discussed in Ref. 8. Plasma parameters for a FIRE AT plasma are discussed in Ref. 9.

The toroidal field is assumed to be 10 [T], and the plasma current I_p is ramped to a flattop value of 7.7 [MA] for 20 [s], as shown in Fig. 2. The area-integrated bootstrap current calculated from neoclassical theory [10] for one of the simulations is also shown in the Fig. The q_{MHD} profile at several times is shown in Fig. 3, plotted against the toroidal flux variable, $x \equiv \sqrt{\text{normalized toroidal flux}}$, which is roughly equal to r/a . The relatively rapid ramp-up of I_p and T_e have the result of keeping $q_{MHD} \geq 1.0$ for most of the discharge

The central plasma densities are assumed to ramp-up as shown in Fig. 4. Plasma profiles in the flattop are shown in Fig. 5. The Z_{eff} profile is assumed to be about 1.36. Accumulation of the alpha ash is modeled, as described in Ref. 10, assuming a recycling coefficient of 20 %. The discharge duration is too short for the ash concentration to reach steady state, or to significantly reduce P_{dt} .

The TRANSP plasma analysis code is used to analyze plasmas with either measured or assumed plasma profiles. TRANSP is a fixed-boundary code, so the FIRE plasma boundary is specified by assuming time evolutions of the major and minor radii, elongation, triangularity, and vertical displacement of the boundaries. The MHD equilibria are calculated in TRANSP by solving the Grad-Shafranov equation. The heat and particle fluxes are calculated from the continuity equations. The fusion alpha particles and beam ions are treated using Monte Carlo methods [6] to model their source rates, neoclassical orbits, and slowing-down rates.

The Kadomstev sawtooth mixing model is used to helically mix the current and temperatures if $q_{MHD}(0)$ is less than unity at sawtooth breaks, assumed to occur with a period of 1 s. Examples of results for the computed $q_{MHD}(0)$ for four simulations are shown in Fig. 6. These four are from a scan with the Greenwald ratio $f_{GW} = \bar{n}_e/\bar{n}_{Greenwald}$ varied. With the plasma startup assumed, only one of the plasmas has sufficient time for $q_{MHD}(0)$ to decrease below unity. The simulated plasmas with low pedestal temperature have sawteeth throughout the flattop.

An example of the evolutions of the central T_e and T_i for one of the plasmas are shown in Fig. 7. The GLF23 prediction starts at 5 s. At that time, the central temperatures drop from their guessed values, then rise again with the start of the ICRH at 6 [s]. They continue to rise until about 27 [s], when the density starts to ramp down.

The predictions start from an assumed boundary temperature, nominally at the top of the H-mode pedestal. Here, this boundary is assumed to occur at $x = 0.95$. The evolution of the

assumed pedestal temperature is shown in Fig. 7. Note that it is not held fixed in time. A scan was done with the pedestal temperature held at 5.4 keV, with the density scaled. Results for the T_i at the time of peak value is shown in Fig. 8. During this scan f_{GW} varied from 0.29 to 0.66. The resulting peak values for P_{dt} and β_n are plotted in Fig. 9. Since the auxiliary heating power at that time is $P_{RF} + P_{Oh} = 11.5 + 1.0$ [MW], the Q_{dt} is greater than 10 for $\bar{n}_e/\bar{n}_{Greenwald} \geq 0.40$.

Lastly, $\bar{n}_e/\bar{n}_{Greenwald}$ is held fixed at 0.66 and the pedestal temperature is scanned down to 2.4 [keV]. The resulting profiles for T_i at the peak are shown in Fig. 10. The values for T_e are shown in Fig. 11. The values for P_{dt} and β_n are plotted in Fig. 12. Thus a pedestal temperature of about 2 [keV] appears sufficient to achieve $Q_{dt} \geq 10$. Results are given in Table 1.

3. ITER-FEAT plasmas

ITER-FEAT [2] is designed to have super-conducting magnets for long pulse duration, and a single-null divertor geometry. The plasma is assumed to be in the ELMy H-mode regime with a n_e profile close to those in Ref. [2] with a target DT fusion yield of $P_{DT} = 400$ [MW]. The n_e profile has the same shape as the FIRE plasma (Fig. 5), with a central value ramped up to $1.02 \times 10^{20}/m^3$ during the flattop.

The assumed ICRH and NNBI heating powers and durations are shown in Fig. 13. The NNBI injection is assumed to be in the plasma current direction at a tangency radius of 6 m. The toroidal rotation of the thermal plasma during the NNBI is computed, assuming $\chi_{mom} = \chi_i$, to peak at 15 krad/s, corresponding to a central Mach number (ratio of velocity and thermal speed) of 0.1. The ratio the central rotation and Alfvén speeds is 1.1-1.4% during the NNBI.

Two values for the flattop temperature pedestal (at $x = 0.85$) were used, 3.9 and 5.1 keV. Several assumptions for the helium ash transport were assumed,

$$\Gamma_{ash} = (-D_{ash}\nabla n_{ash} + V_{ash}n_{ash})A_{surf}, \quad (1)$$

with A_{surf} the area of the flux surface at x , $D_{ash} = 0.5$ or 0.8 m^2/s , and $V_{ash} = 0$ or -0.1 m/s.

After the ICRH and NNBI are stopped, P_{dt} and the alpha heating continue to increase slowly, as shown in Fig. 13. The temperature profiles from two simulations with different pedestal temperatures are shown in Fig. 14. As expected for relatively stiff transport models such as GLF23, the central temperatures and P_{dt} increase with pedestal temperature. The sawtooth mixing radius increases slowly as $T_e(0)$ increases. Sawtooth mixing reduces the alpha ash in the center, and the concentration does not reach equilibrium after 400 s. Results are summarized in Table 2.

4. Summary and Discussion

This paper reports results for self-consistent transport simulations of burning plasmas for FIRE and ITER-FEAT using the GLF23 model incorporated into the TRANSP analysis code. Relatively flat density profiles are assumed for both. ICRH is assumed for both, and NNBI is assumed for ITER-FEAT. For FIRE with the assumed heating, the plasmas achieve $Q_{dt} \geq 10$ for $\bar{n}_e/\bar{n}_{Greenwald} = 0.66$ with pedestal temperatures as low as 2.5 [keV]. For the ITER-FEAT plasmas, the predicted central temperatures continue to increase slowly with P_{dt} after the ICRH and NNBI are stopped.

The results for P_{dt} and Q_{dt} depend sensitively on the pulse durations. The relatively short pulse durations in FIRE ($\simeq 20$ s) imply that the pedestal temperature is a key parameter. The relatively long (> 300 s) imply that very large Q_{dt} could be anticipated, and that P_{dt} will depend sensitively on details of the ash transport and on sawtooth mixing.

5. Acknowledgments

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TRANSP run ID	$\bar{n}_e/\bar{n}_{Greenwald}$	β_n	T_{ped}	P_{dt}	P_α	$\tau_E(0.95)$	$\tau_{98,y}(0.95)$
units			[keV]	[MW]	[MW]	[s]	[s]
50000G07	0.29	1.30	5.4	81.7	16.2	0.89	0.68
50000G09	0.44	1.90	5.4	169	34.2	0.81	0.56
50000G10	0.58	2.52	5.4	287	58.0	0.73	0.47
50000G13	0.66	2.83	5.4	355	72.0	0.67	0.42
50000G14	0.66	2.46	4.5	285	56.0	0.71	0.50
50000G15	0.66	1.75	2.72	152	30.0	0.83	0.74
50000G18	0.66	1.40	2.06	94.5	18.5	0.94	0.94
50000G17	0.66	0.98	1.35	36	7.2	0.90	1.20

Table 1. Summary of FIRE plasma parameters at a steady state time (26.5 s).

TRANSP run ID	T_{ped}	D_{ash}	V_{ash}	$\int dV n_{ash}$	β_n	P_{dt}
units	[keV]	[m^2/s]	[m/s]	[10^{20}]		[MW]
03000G03	3.6	0.8	0	1.8	1.54	332
03000G04	3.9	0.8	-0.1	4.5	1.51	313
03000G05	5.1	0.8	0	2.4	1.86	451
03000G06	5.1	0.8	-0.1	6.2	1.66	425
03000G08	5.1	0.5	0	2.44	1.85	442

Table 2. Summary of ITER-FEAT plasma parameters at 300 s.

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- [10] W. Houlberg, K. Shang, S. Hirshman, and M. Zarnstorff, *Phys. Plasmas* 4 (1997) 3230.

Figure Captions

- Fig. 1 - Evolution of the heating powers in a FIRE plasma.
- Fig. 2 - Evolution of the assumed total current and computed I_{boot} in a FIRE plasma.
- Fig. 3 - Profile of q_{MHD} for one of the FIRE plasmas.
- Fig. 4 - Evolution of the assumed central density in a FIRE plasma.
- Fig. 5 - Density profiles at a flattop time.
- Fig. 6 - Evolution of q_{MHD} with various Greenwald fractions.
- Fig. 7 - Evolution of central and pedestal temperatures for one of the FIRE plasmas.
- Fig. 8 - Scaling of T_i with Greenwald fraction.
- Fig. 9 - Scaling of dt fusion power with Greenwald fraction in FIRE plasma with $T_{ped} = 5.4$ KeV.
- Fig.10 - Scaling of q_{MHD} with the pedestal Temperature.
- Fig.11 - Scaling of T_e with the pedestal Temperature.
- Fig.12 - Scaling of dt fusion power with T_{ped} .
- Fig.13 - Heating powers for ITER-FEAT with $T_{ped} = 5.1$ keV.
- Fig.14 - Temperature profiles from two simulations of ITER-FEAT with different pedestal temperatures.
- Fig. 15 - Helium ash profiles in ITER-FEAT before and after a sawtooth crash.

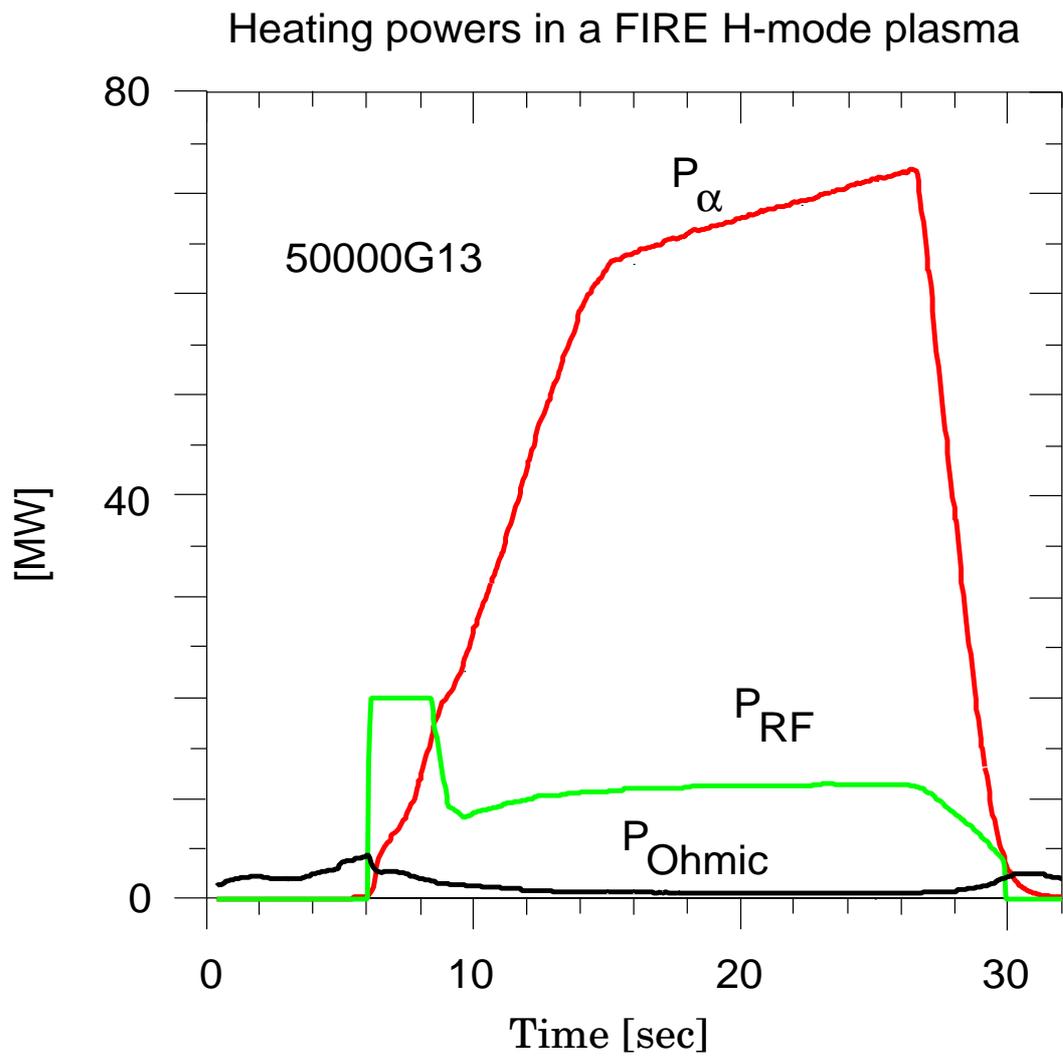


Figure 1. Evolution of the heating powers in a FIRE plasma.

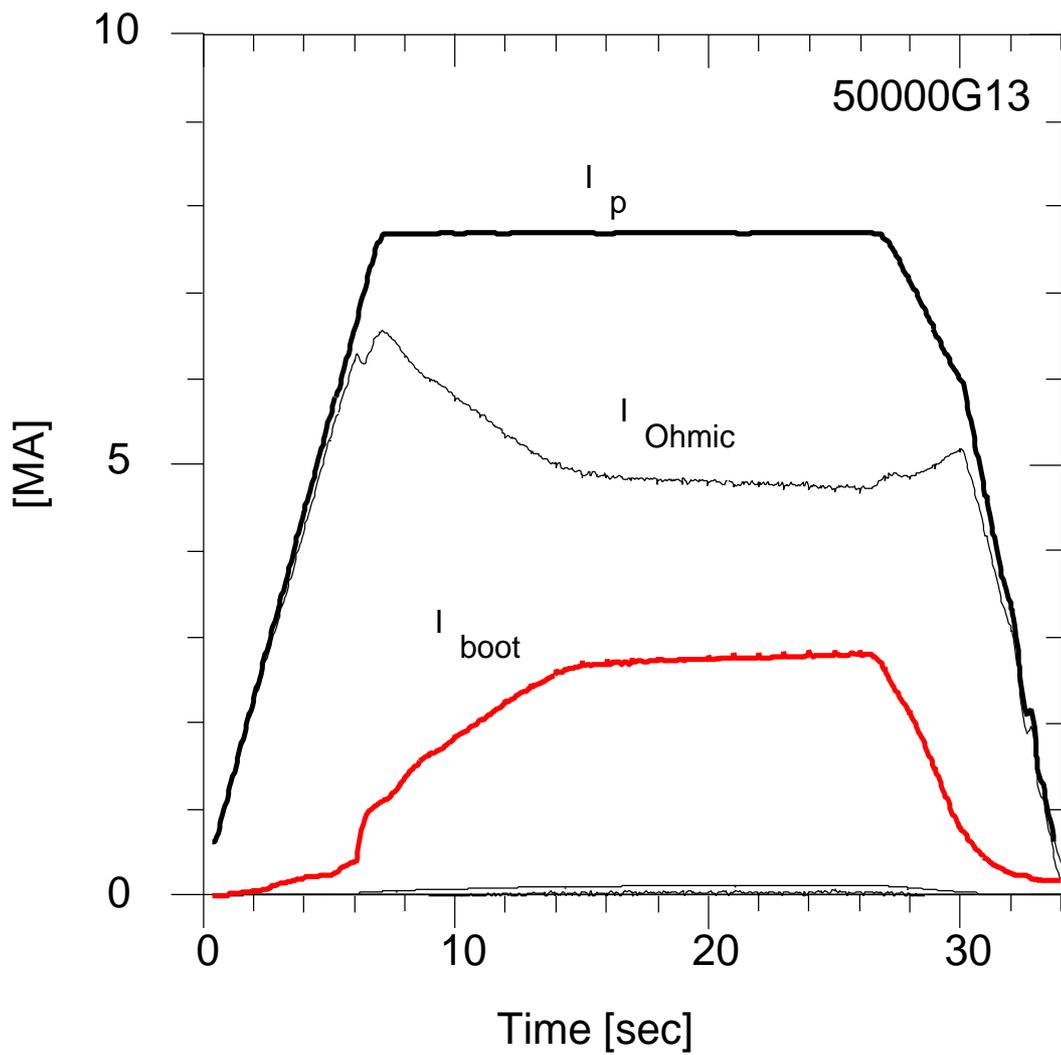


Figure 2. Evolution of the assumed total current and computed I_{boot} in a FIRE plasma.

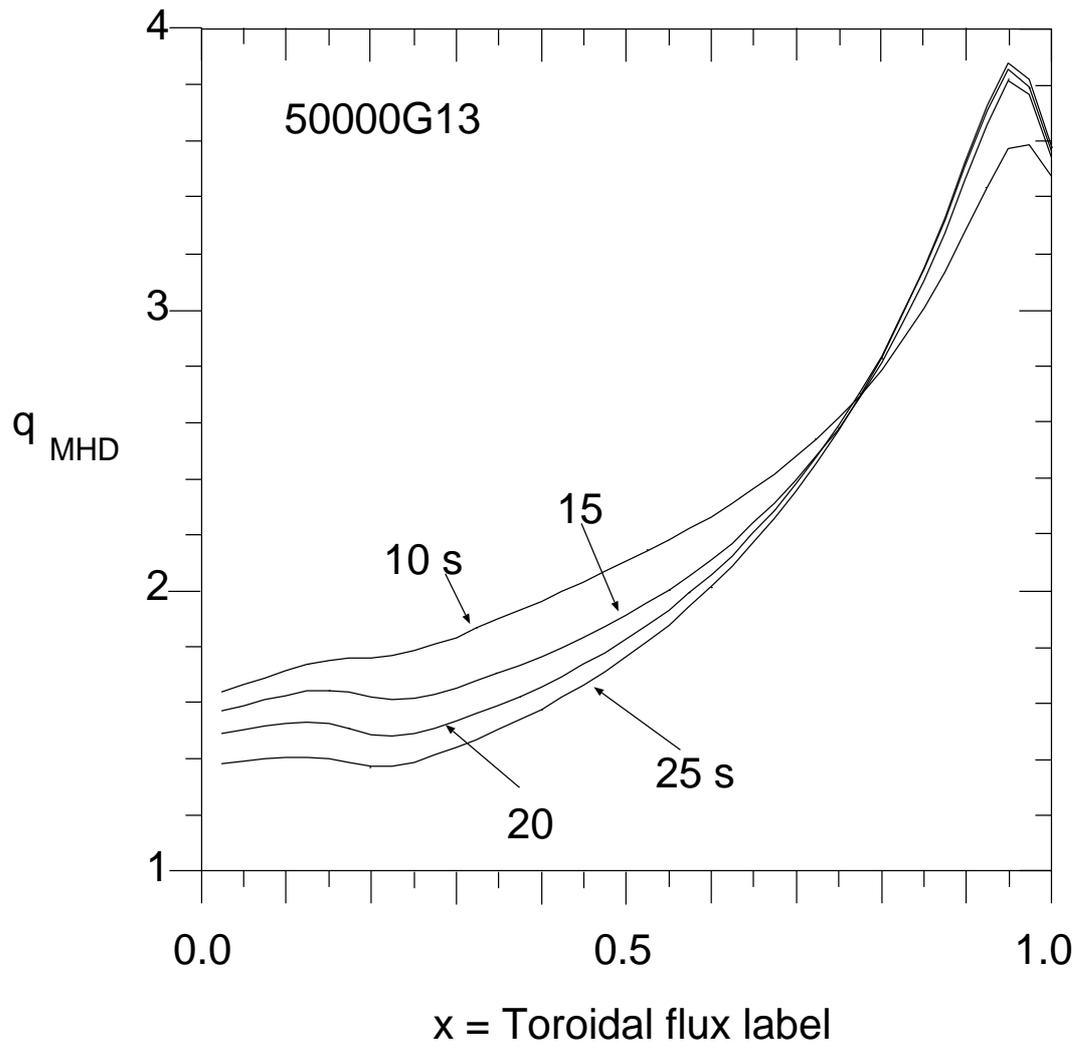


Figure 3. Profile of q_{MHD} for one of the FIRE plasmas.

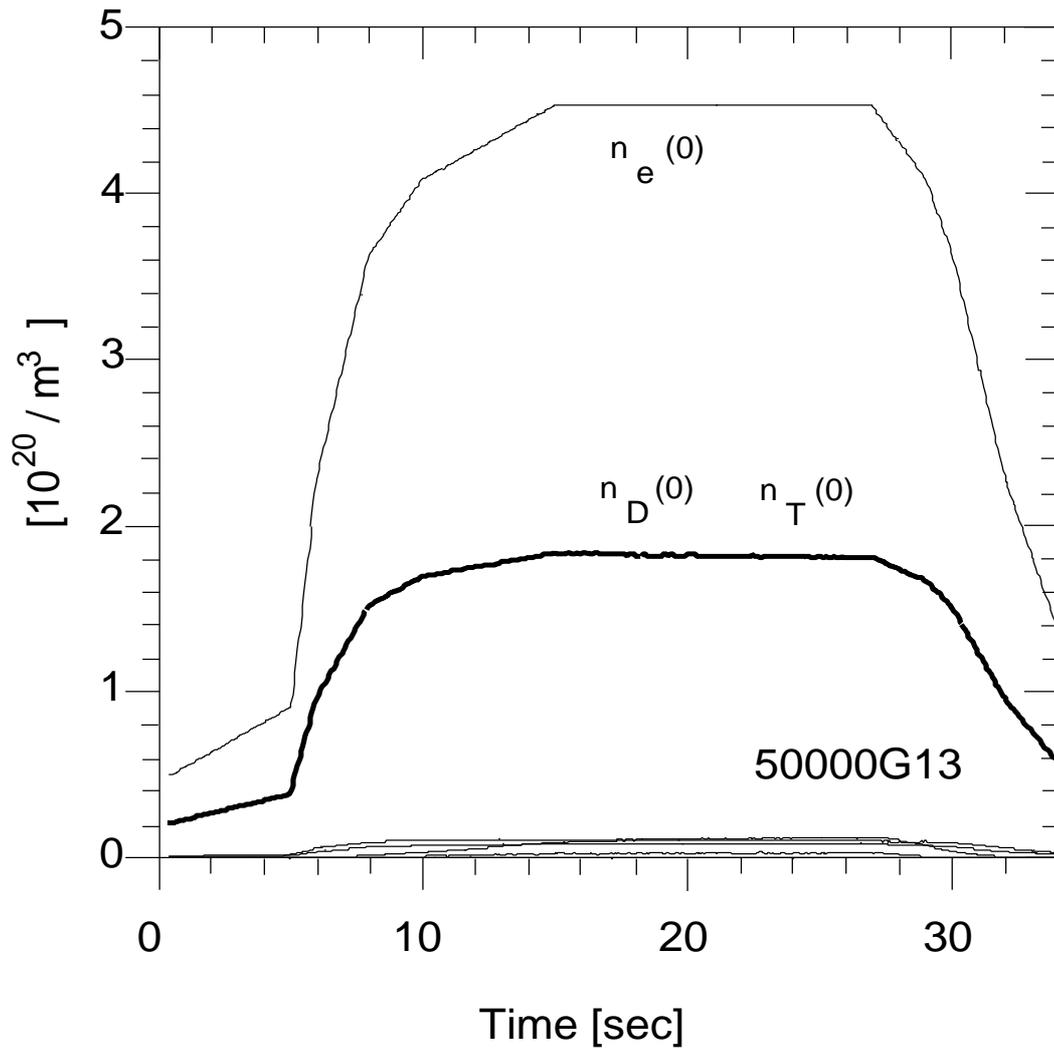


Figure 4. Evolution of the assumed central density in a FIRE plasma.

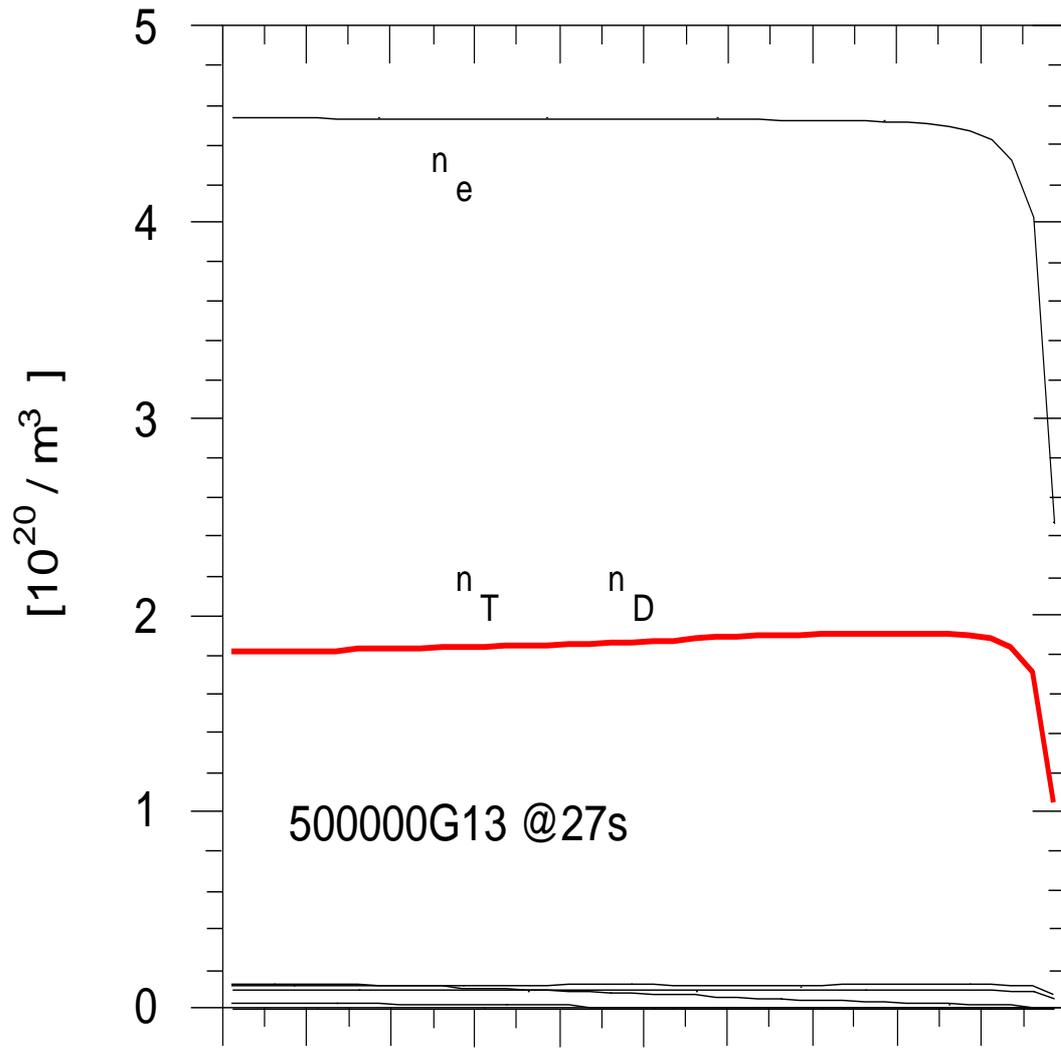


Figure 5. Density profiles at a flattop time.

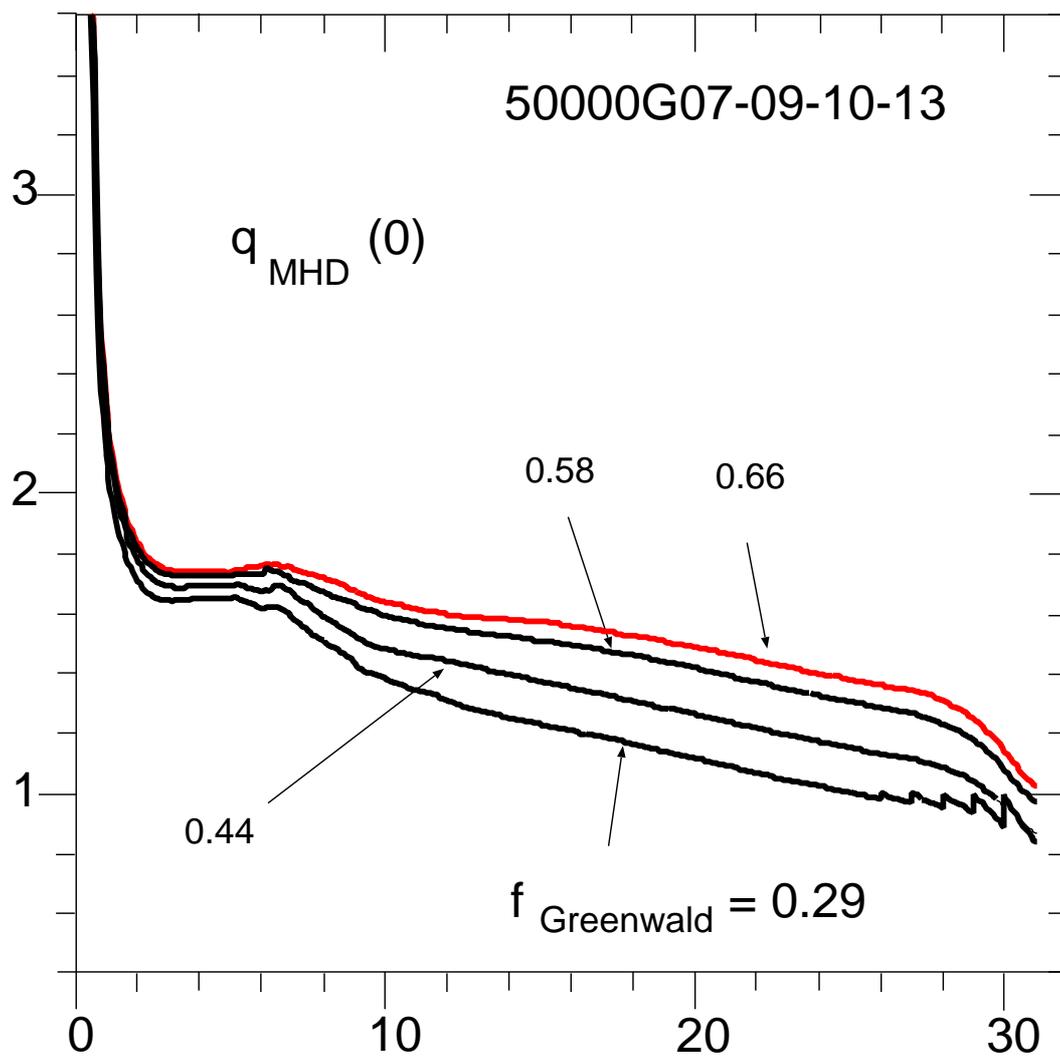


Figure 6. Evolution of q_{MHD} with various Greenwald fractions.

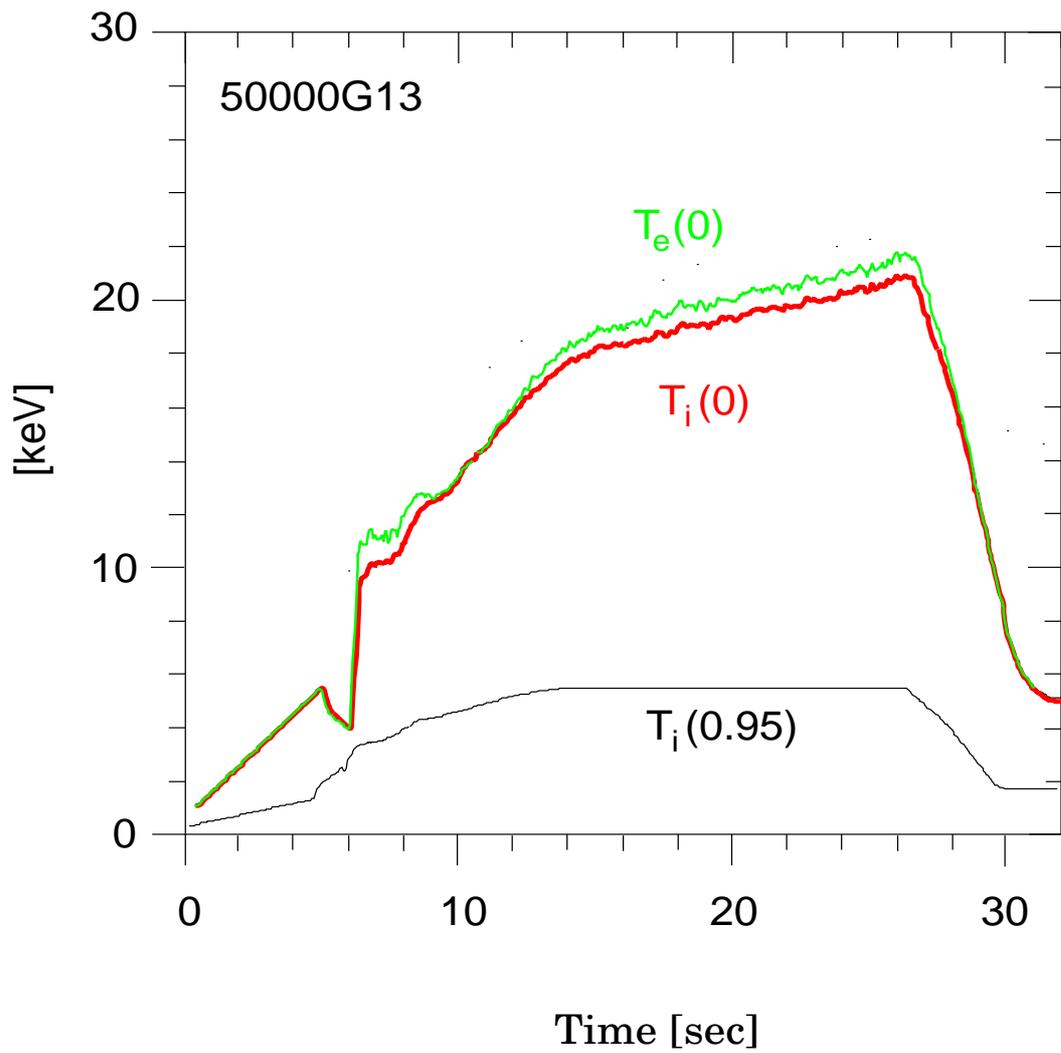


Figure 7. Evolution of central and pedestal temperatures for one of the FIRE plasmas.

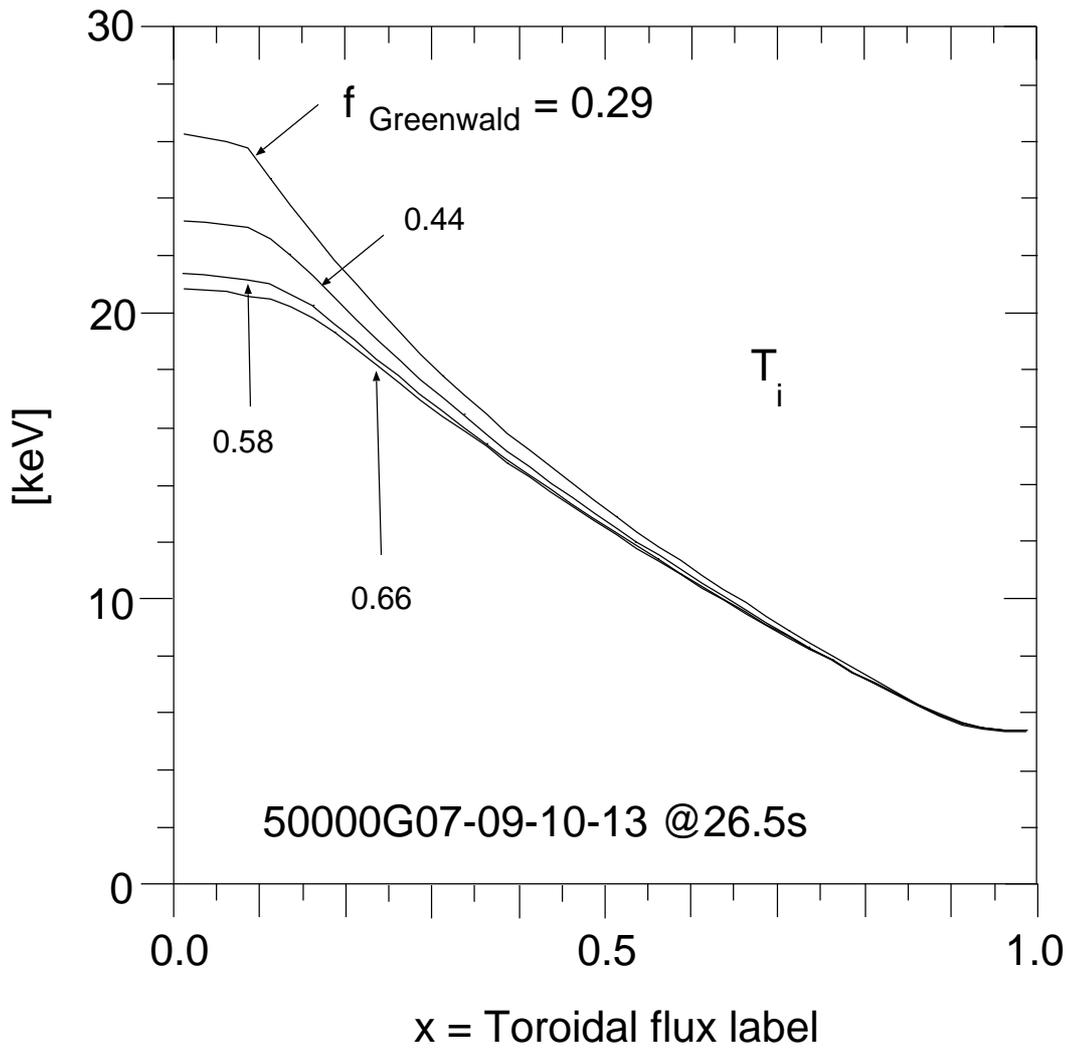


Figure 8. Scaling of T_i with Greenwald fraction.

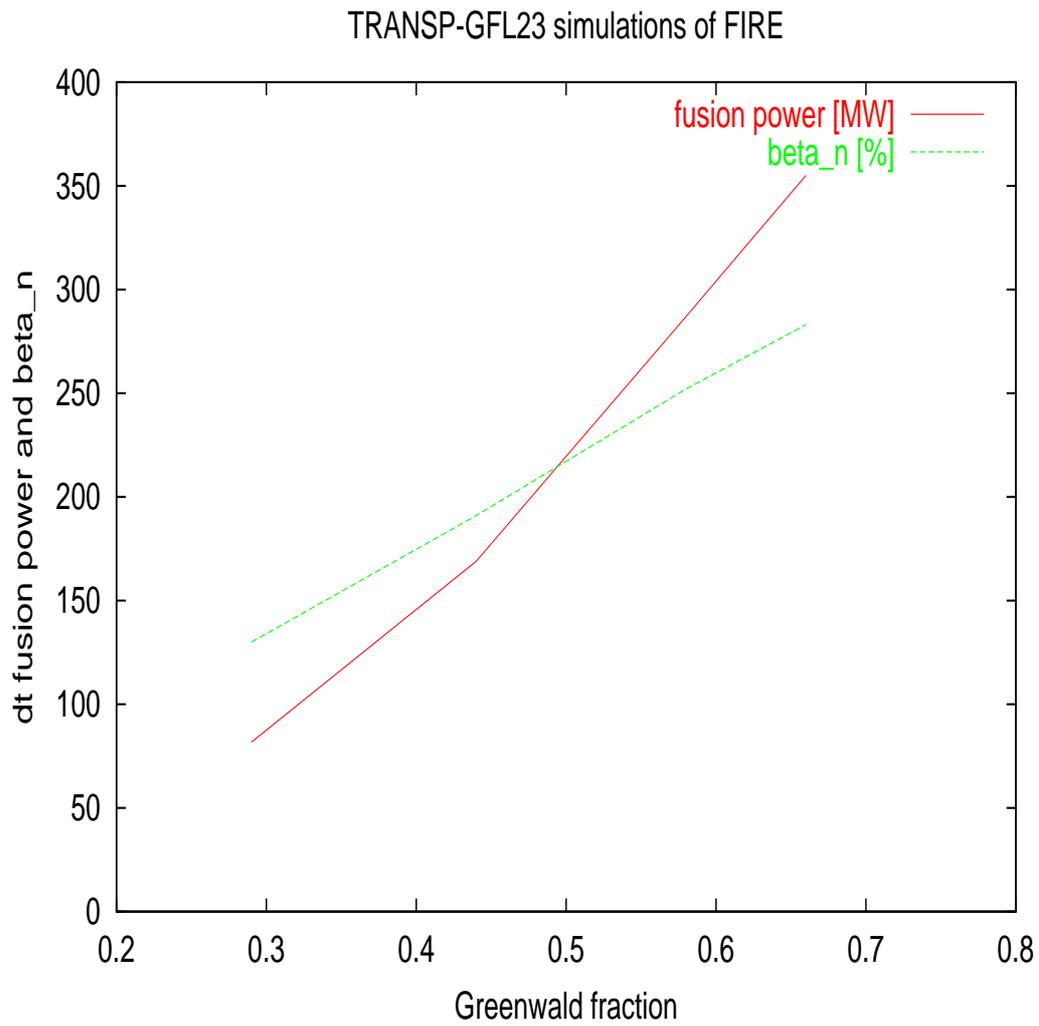


Figure 9. Scaling of dt fusion power with Greenwald fraction in FIRE plasma with $T_{ped} = 5.4$ KeV.

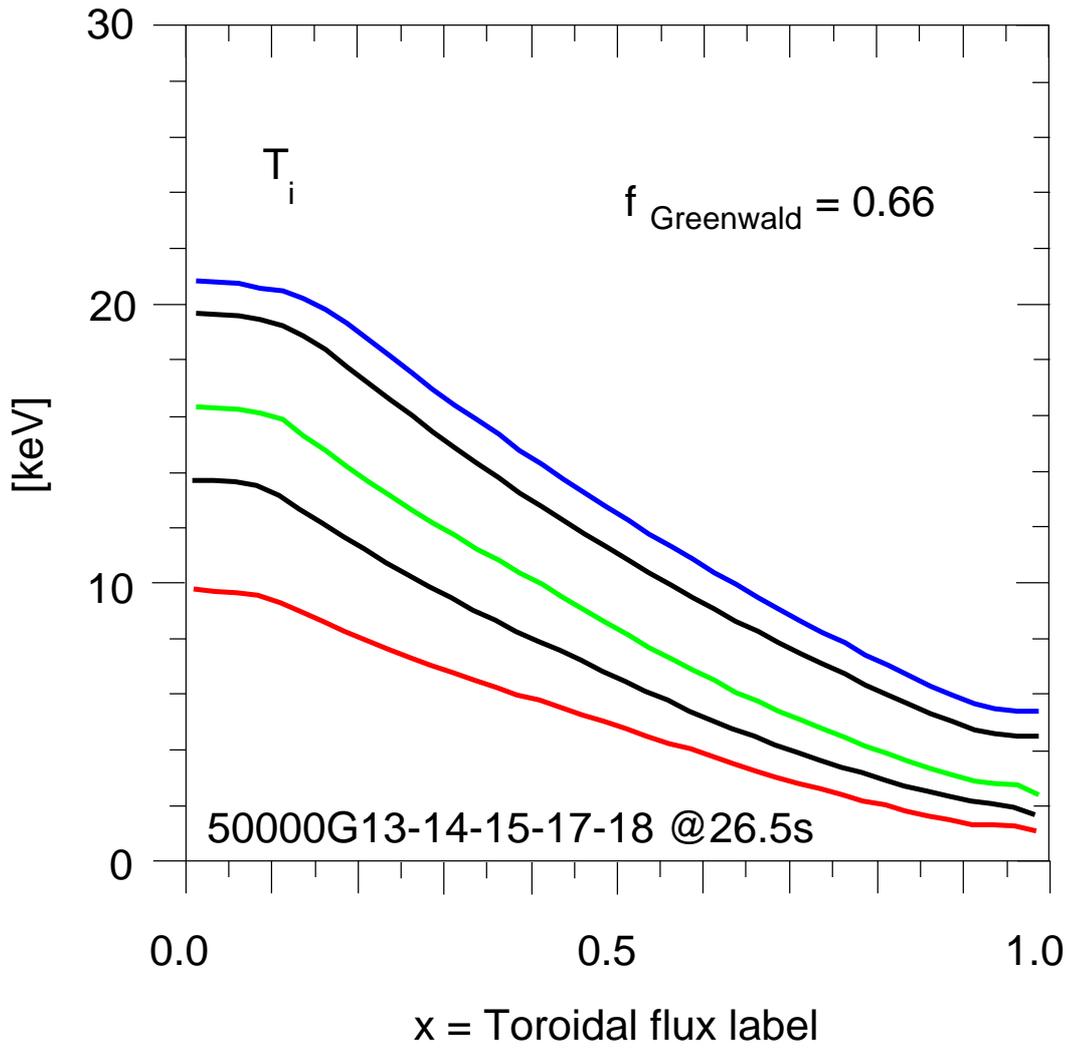


Figure 10. Scaling of with the pedestal Temperature.

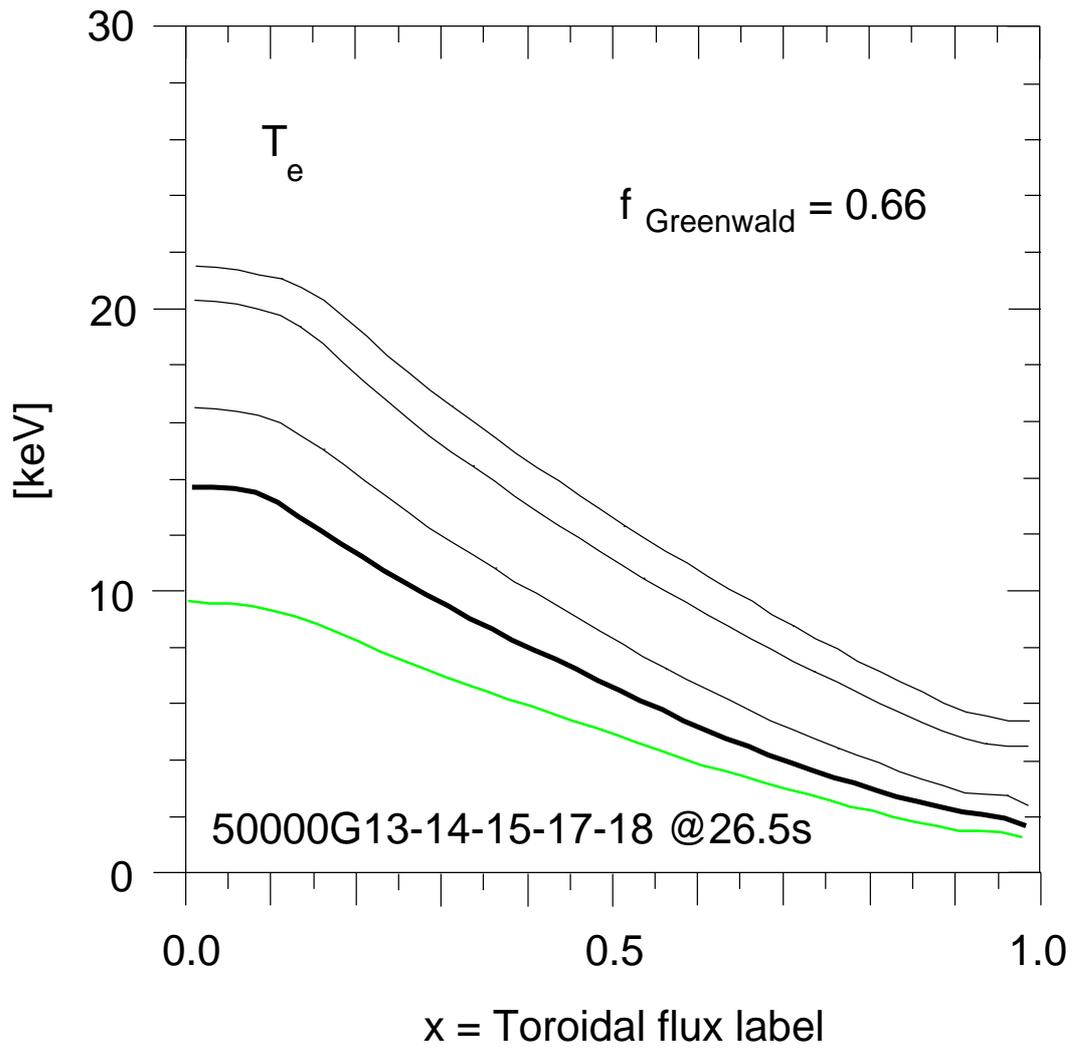


Figure 11. Scaling of T_e with the pedestal Temperature.

TRANSP-GFL23 simulations of FIRE

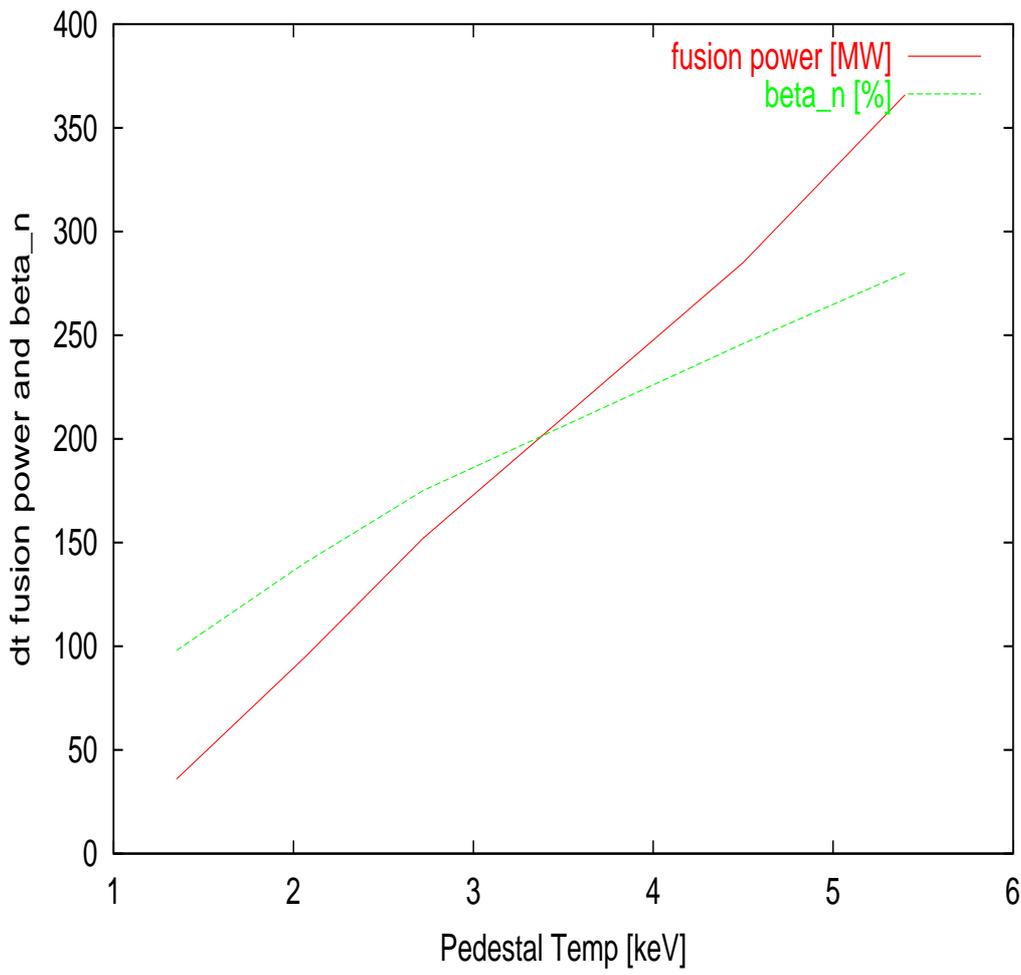


Figure 12. Scaling of dt fusion power with T_{ped} .

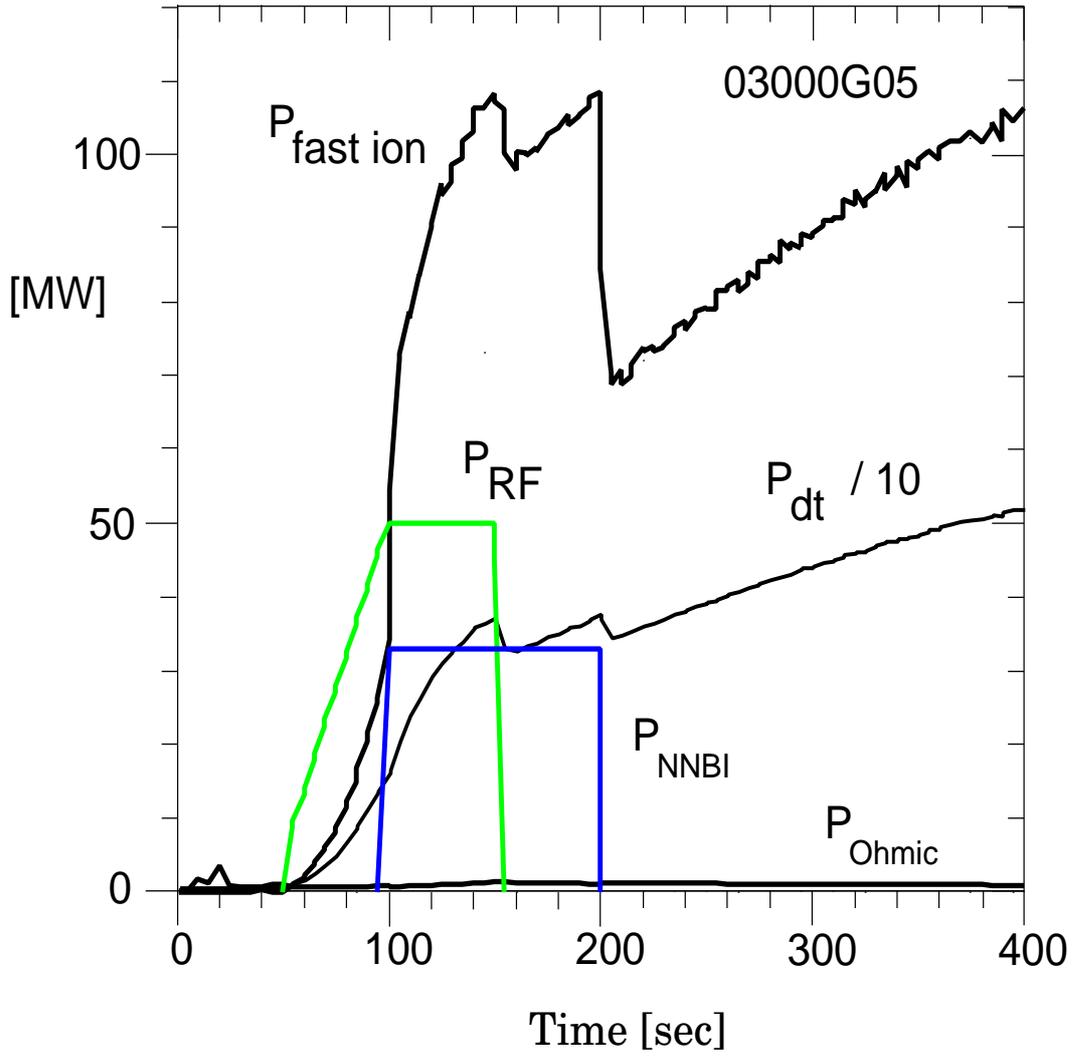


Figure 13. Heating powers for ITER-FEAT with $T_{ped} = 5.1 \text{ keV}$.

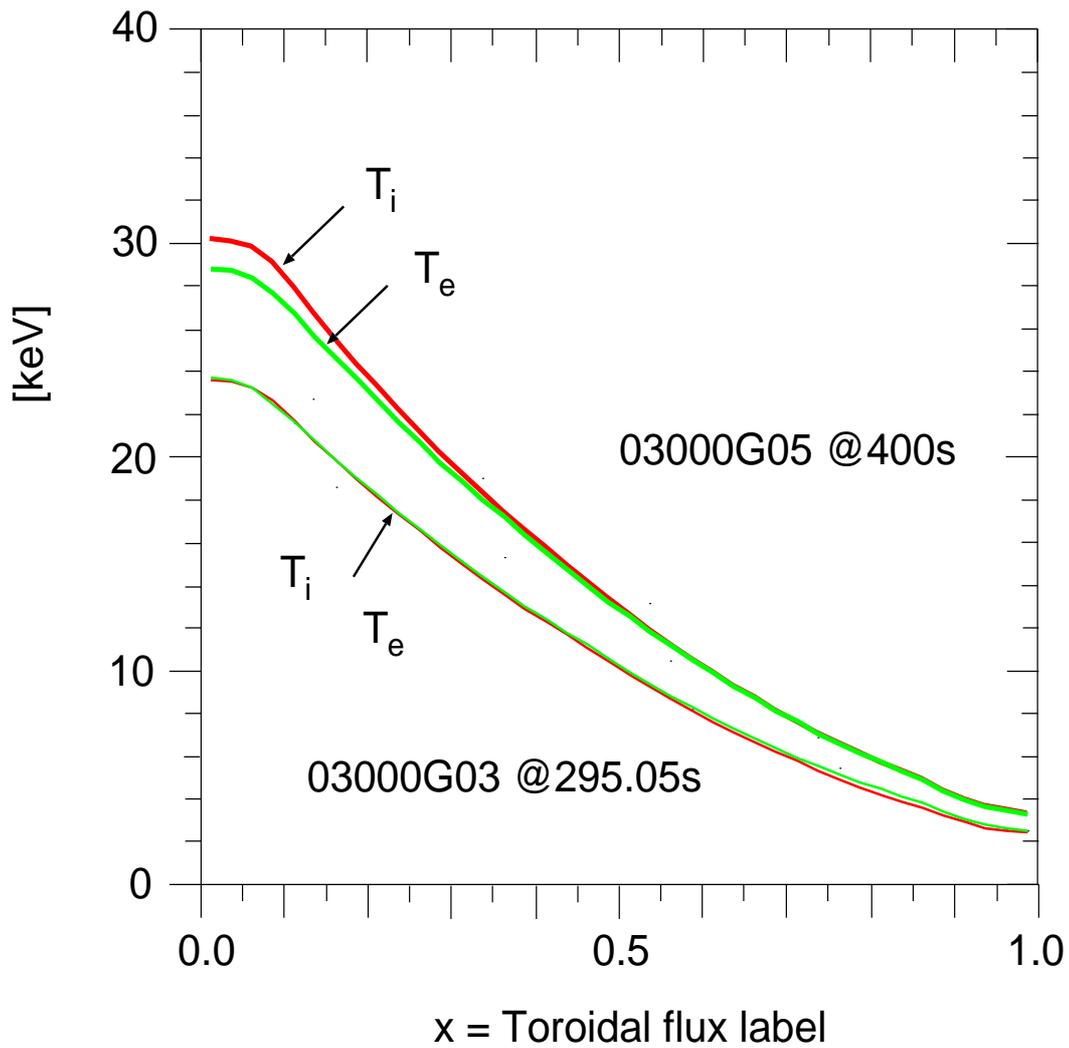


Figure 14. Temperature profiles from two simulations of ITER-FEAT with different pedestal temperatures.

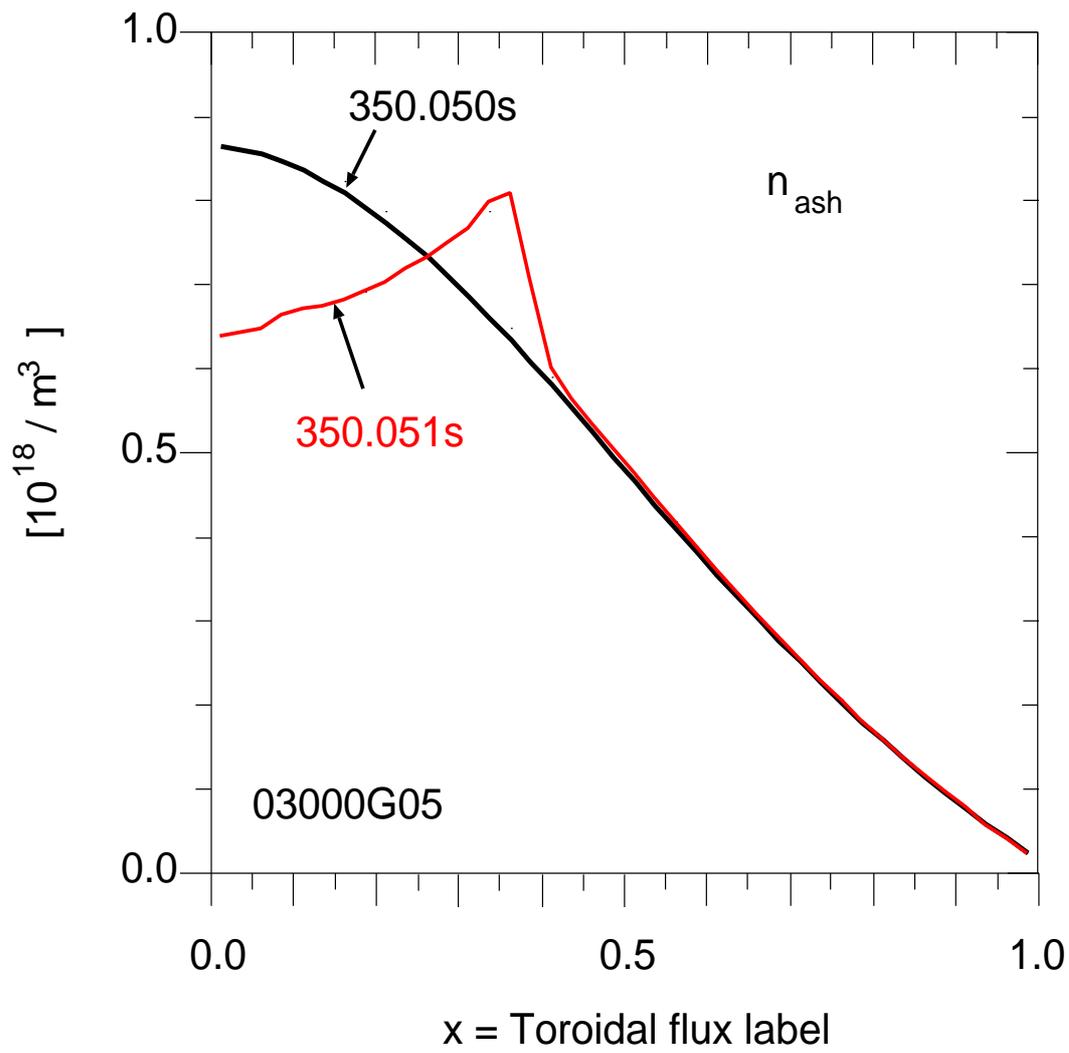


Figure 15. Helium ash profiles in ITER-FEAT before and after a sawtooth crash.

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